

# A Steady-State Isotopic Transient Kinetic Analysis of the NO/O<sub>2</sub>/H<sub>2</sub> Reaction over Pt/SiO<sub>2</sub> Catalysts

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The NO/O<sub>2</sub>/H<sub>2</sub> reaction under strongly oxidising conditions has been studied over a 5% Pt/SiO<sub>2</sub> catalyst using Steady-State Isotopic Transient Kinetic Analysis (SSITKA). The <sup>14</sup>N-containing reactants and products were monitored following a <sup>14</sup>NO/O<sub>2</sub>/H<sub>2</sub> → <sup>15</sup>NO/O<sub>2</sub>/H<sub>2</sub> switch. N<sub>2</sub>O was found to be the isotopically first product and N<sub>2</sub> the isotopically second. It was found that there was a constant desorption of NO from the catalyst surface under steady-state conditions. Recently introduced transformations (IDIMP, TRIMP, and the semilogarithmic plot of the  $\bar{\alpha}$  function versus time) of the product profiles, which concentrate on the isotopic distribution of the product molecules following the <sup>14</sup>NO → <sup>15</sup>NO switch, are used to analyse the mechanism of N<sub>2</sub> formation from this reaction. These show that N<sub>2</sub> formation is predominantly through an “impact” route in which gaseous or physisorbed NO reacts with a reduced N species on the catalyst in a modified Eley–Rideal mechanism. A second, less active, mode of N<sub>2</sub> formation is through the interaction of two equivalent species on the surface, each of which gives one N atom to the N<sub>2</sub> molecule. The presence of O<sub>2</sub> results in a change in the relative contribution of each type of N<sub>2</sub> production.

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**Key Words:** NO<sub>x</sub> reduction; H<sub>2</sub> reductants; lean burn; SSITKA.

## INTRODUCTION

NO<sub>x</sub> removal using hydrocarbon reductants in an oxidising environment has attracted recent attention (1, 2) for after-treatment systems for diesel and lean-burn gasoline engines (3, 4). Pt catalysts seem most promising (5, 6), and various reductants (CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub>, C<sub>3</sub>H<sub>6</sub>, C<sub>3</sub>H<sub>8</sub>, C<sub>8</sub>H<sub>18</sub>) (7, 8) have been studied. It has been found that the reaction mechanism and hence the activity for the deNO<sub>x</sub> reaction is strongly dependent on the choice of reductant.

H<sub>2</sub> is not, in general, a selective reductant since it reacts preferentially with O<sub>2</sub> rather than with NO<sub>x</sub> (9). However, it has recently been found that the reduction of NO<sub>x</sub> in an oxidising environment can be performed with H<sub>2</sub> on Pt catalysts at low temperatures. The formation of N<sub>2</sub>O remains a

problem, however, and it is found that at low temperatures the selectivity to N<sub>2</sub>O can be over 50% (10–13).

SSITKA is a valuable technique (14, 15) which can be used for the determination of the number and activity of catalytic sites on a catalyst under *actual* reaction conditions (16–18). It has been used, for example, to study the Fischer–Tropsch reaction (19) and the selective reduction of NO using CH<sub>4</sub> (20). Generally, the reactions from which most information is gained are those in which there are large reservoirs of relatively inert surface intermediates which form product molecules.

We have previously used the SSITKA technique to study the NO/C<sub>3</sub>H<sub>6</sub>/O<sub>2</sub> (21) and the NO/H<sub>2</sub> (11) reactions over supported Pt catalysts and, using mathematical modelling techniques, have developed several criteria for the analysis of the product profiles in order to obtain information about the nature of surface intermediates, and thus an improved understanding of the reaction mechanism (11).

Since the development of the SSITKA technique there have been numerous papers devoted to the numerical analysis of SSITKA profiles with the aim of generating information about reaction mechanisms. These numerical analyses have generally taken the form of modelling the transient data generated from either continuously stirred tank (22, 23) or plug flow (24) reactors. Comprehensive reviews of the technique have been published (14, 15). However, it is generally the case that most workers have analysed isotope transfer only, i.e., the fraction of isotopes within the reactant and product components with time. Distribution of isotopic molecules has been disregarded or only partially considered without detailed qualitative analysis of experimental data (25).

In this paper we describe several methods of analysing the data obtained from isotopic transients in order to try to develop information about the reaction mechanism. Some features of these methods originally come from classical isotopic exchange analysis in closed systems without the occurrence of chemical changes in the system (26–33). We have extended these analyses to SSITKA studies for use in a flow system with the occurrence of chemical change.

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Specifically, our approach will be for situations where a reactant molecule ( $RA_n$ ) containing labelled atoms (where there are two possible isotopes for the A element) is converted, via intermediates ( $IA_x$ ), into a product molecule that contains two such labelled atoms ( $PA_2$ ) for a steady-state reaction in a plug flow reactor, e.g.,  $^*NO + H_2 \rightarrow ^*N_2/^*N_2O$ , where \* represents a labelled atom. A full mathematical description of the methodology used in the interpretation and modelling of these results is presented elsewhere (34). Only the essential details are given here.

## EXPERIMENTAL

The catalytic system used in this study has been described fully elsewhere (21). The catalyst is 5% Pt/SiO<sub>2</sub> prepared by incipient wetness from a Pt(DNDA) solution. The surface area of the catalyst was  $\sim 260 \text{ m}^2 \text{ g}^{-1}$  and the metal dispersion was 31%, corresponding to an exposed metal surface of  $4.74 \times 10^{19} \text{ atoms g}^{-1}$  ( $3.78 \text{ m}^2 \text{ g}^{-1}$ ). These values were measured using an "in-house" BET and H<sub>2</sub>-chemisorption apparatus. One hundred and thirteen milligrams of the catalyst was placed in a quartz reactor tube, preceded by 100 mg of quartz chips which preheated the incoming gas (particle size, 250–850  $\mu\text{m}$ ; reactor diameter, 4 mm). The reaction mixture was 1.64% NO, 1.64% H<sub>2</sub>, 8.7% O<sub>2</sub>, in an He carrier gas at a total flow of  $113 \text{ cm}^3 \text{ min}^{-1}$ .

The temperature programmed reaction was carried out after the catalyst was pretreated in the reaction mixture for 1 h at 400°C and the catalyst was cooled in the reaction mixture and ramped in He to 500°C at a rate of  $5^\circ\text{C min}^{-1}$ . The effluent was continuously monitored for NO, NO<sub>2</sub>, N<sub>2</sub>, N<sub>2</sub>O, H<sub>2</sub>O, and NH<sub>3</sub>, as the temperature was ramped, using a "Gaslab" mass spectrometer. The absolute amounts of desorbed products were calculated using calibration plots of mass spectrometer responses against partial pressure.

The SSITKA switches involved taking a catalyst to a steady state in <sup>14</sup>NO/O<sub>2</sub>/H<sub>2</sub> and then switching out the <sup>14</sup>NO and replacing it with an equivalent flow (and pressure) of <sup>15</sup>NO. The original flow of <sup>14</sup>NO also contained a 5% Ar tracer, the decay in which was used to monitor the gas-phase holdup of the system ( $\sim 1.5 \text{ s}$ ). Differences between the pressures of the lines arise from the fact that the gas that is being used as a reactant is flowing through the catalyst and thus experiences some back-pressure. The pressure in the <sup>14</sup>NO and <sup>15</sup>NO lines are measured using two "Wika" pressure transducers and are equalised using a fine needle valve.

Following this switch, the reactor effluent is continuously monitored for all isotopic molecules of NO (at  $m/e = 30$  and 31), N<sub>2</sub> (at 28 and 29), NO<sub>2</sub> (at 46 and 47), and N<sub>2</sub>O (at 44 and 45). Overlaps in the  $m/e = 30$  and  $m/e = 46$  peaks (where <sup>14</sup>NO and <sup>15</sup>N<sub>2</sub> and <sup>15</sup>N<sub>2</sub>O and <sup>14</sup>NO<sub>2</sub> share  $m/e$  values) are allowed for by considering that the overall production of N<sub>2</sub> and N<sub>2</sub>O are not changed by the switch from <sup>14</sup>NO to <sup>15</sup>NO. Thus the relevant profiles for <sup>15</sup>N<sub>2</sub> and <sup>15</sup>N<sub>2</sub>O can be

mathematically generated using the fact that the normalised production of N<sub>2</sub> and N<sub>2</sub>O at any time following the switch must equal 1. In a similar manner the profile for the upcoming <sup>15</sup>NO<sub>2</sub> species following the <sup>14</sup>NO  $\rightarrow$  <sup>15</sup>NO switch is used to calculate the expected decrease in the <sup>14</sup>NO<sub>2</sub> signal.

The use of the reverse switch, i.e., <sup>15</sup>NO  $\rightarrow$  <sup>14</sup>NO, after a prolonged period in the <sup>15</sup>NO/O<sub>2</sub>/H<sub>2</sub> reaction mixture allows the measurement of upcoming <sup>14</sup>N<sub>2</sub> and <sup>14</sup>N<sub>2</sub>O profiles, which are what would be expected for the <sup>15</sup>N<sub>2</sub> and <sup>15</sup>N<sub>2</sub>O profiles from the original <sup>14</sup>NO  $\rightarrow$  <sup>15</sup>NO switch. These profiles are approximately the same as those mathematically generated by the above-mentioned process.

For the TRIMP, IDIMP, and semilogarithmic analyses (see below) the experiment was modified in order to further minimise the pressure change. This was achieved by reducing the overall flow rate to  $73 \text{ cm}^3 \text{ min}^{-1}$ , leading to a gas composition of 2.5% NO, 2.5% H<sub>2</sub>, 14.8% O<sub>2</sub> in an He flow. This experiment was performed at 70°C.

## RESULTS

### Temperature Programmed Reaction

Figure 1 shows the production of N<sub>2</sub>, N<sub>2</sub>O, and NO<sub>2</sub> as a function of temperature. This profile is in qualitative agreement with that measured under steady-state conditions (10). The production of N<sub>2</sub>O peaks at  $\sim 100^\circ\text{C}$  while the N<sub>2</sub> reaches a broad maximum between  $\sim 110$  and  $140^\circ\text{C}$ . The production of NO<sub>2</sub> is seen at temperatures lower and higher than the maxima in the N<sub>2</sub>O and N<sub>2</sub> profiles. The

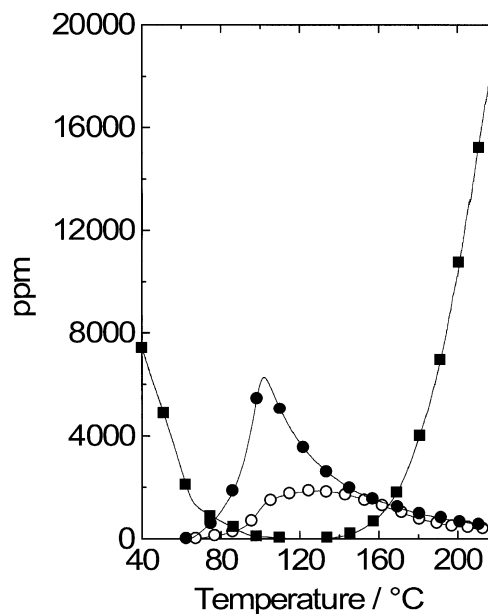


FIG. 1. Temperature programmed reaction of NO/H<sub>2</sub>/O<sub>2</sub> over a 5% Pt/SiO<sub>2</sub> catalyst. The reactant stream contained 1.64% NO, 1.64% H<sub>2</sub>, and 8.7% O<sub>2</sub> with an He carrier gas in a total flow of  $113 \text{ cm}^3 \text{ min}^{-1}$  and catalyst mass = 113 mg: N<sub>2</sub> (○), N<sub>2</sub>O (●), and NO<sub>2</sub> (■).

lower temperature formation of NO<sub>2</sub> is due to the gas-phase interaction of NO molecules with O<sub>2</sub> molecules. The higher temperature production of NO<sub>2</sub> is ascribed to the interaction of NO<sub>(g)</sub> with O<sub>ads</sub> on the catalyst surface.

The trend in selectivity for the N<sub>2</sub> and N<sub>2</sub>O products is the same as that observed previously for the NO/H<sub>2</sub> reaction (11). The catalyst is far more selective to N<sub>2</sub>O than to N<sub>2</sub> at these temperatures. In contrast to the NO/H<sub>2</sub> reaction no NH<sub>3</sub> is formed. This is reasonable because the gas phase is oxidising and NH<sub>3</sub> would only be expected to be formed under reducing conditions.

### Steady-State Isotopic Transient Kinetic Analysis

Two temperatures (60 and 83°C), where the conversion of NO was quite low, were chosen for the SSITKA of the NO/O<sub>2</sub>/H<sub>2</sub> reaction over the 5% Pt/SiO<sub>2</sub> catalyst. The rates of production of N<sub>2</sub> and N<sub>2</sub>O, as well as the flow rate of unreacted NO under these conditions, as a function of the temperature of reaction, are presented in Table 1. The rates of reaction are calculated from the total observed change in <sup>14</sup>N<sub>2</sub> (or <sup>14</sup>N<sub>2</sub>O) signal upon removal of the <sup>14</sup>NO and insertion of the <sup>15</sup>NO.

It can be seen (Table 1) that the rates of production of N<sub>2</sub> and N<sub>2</sub>O increase as the temperature is raised. Figure 2 shows the normalised isotopic product responses following the <sup>14</sup>NO/H<sub>2</sub>/O<sub>2</sub> → <sup>15</sup>NO/H<sub>2</sub>/O<sub>2</sub> switch over the 5% Pt/SiO<sub>2</sub> catalyst at *T* = 83°C. Plots relating to the Ar (and its inverse) signal are also shown for reference.

The product plots have much in common with profiles observed earlier for the C<sub>3</sub>H<sub>6</sub>/NO/O<sub>2</sub> (21) and NO/H<sub>2</sub> (11) systems. The decrease in production of unlabelled N<sub>2</sub> (Δ) and N<sub>2</sub>O (▲) is instantaneous with the switch, as is the production of mixed-labelled N<sub>2</sub> (○) and N<sub>2</sub>O (●). The mixed-labelled N<sub>2</sub> and N<sub>2</sub>O profiles rise through maxima very shortly after the switch and begin to decrease after this time. A mathematically generated <sup>15</sup>N<sub>2</sub> profile (◇) is also seen to increase from zero shortly after the switch, as is the generated <sup>15</sup>N<sub>2</sub>O profile (◆).

TABLE 1

Rates of Formation of N<sub>2</sub> and N<sub>2</sub>O and the Flow Rate of Unreacted NO (μmol g<sup>-1</sup> s<sup>-1</sup>) over a 5% Pt/SiO<sub>2</sub> Catalyst at Two Temperatures in an NO/O<sub>2</sub>/H<sub>2</sub> Stream

T/°C	<i>r</i> (N <sub>2</sub> )	τ(N <sub>2</sub> )	<i>r</i> (N <sub>2</sub> O)	τ(N <sub>2</sub> O)	<i>r</i> (NO)	τ(NO)
60	0.04	64 ± 0.5	0.46	1.1 ± 0.5	10.01	0.6 ± 0.5
83	0.09	42 ± 0.5	1.27	0.7 ± 0.5	8.53	0.8 ± 0.5

Note. Also shown are values for τ (the mean surface residence time (s)) for the products and reactant as determined from SSITKA analysis. The reactant stream contained 1.64% NO, 1.64% H<sub>2</sub>, and 8.7% O<sub>2</sub> with an He carrier gas in a total flow of 113 cm<sup>3</sup> min<sup>-1</sup> over a 5% Pt/SiO<sub>2</sub> catalyst (113 mg).

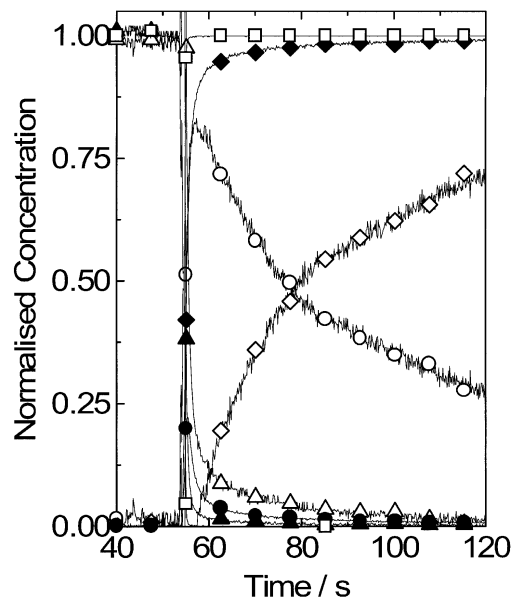


FIG. 2. Normalised product responses following the replacement of <sup>14</sup>NO/Ar with <sup>15</sup>NO in the reaction stream. Reaction conditions: 1.64% NO, 1.64% H<sub>2</sub>, and 8.7% O<sub>2</sub> with an He carrier gas in a total flow of 113 cm<sup>3</sup> min<sup>-1</sup>, catalyst mass = 113 mg, *T* = 83°C. <sup>14</sup>N<sub>2</sub> (Δ), <sup>14</sup>N<sup>15</sup>N (○), <sup>15</sup>N<sub>2</sub> (◇), <sup>14</sup>N<sub>2</sub>O (▲), <sup>14</sup>N<sup>15</sup>N<sub>2</sub>O (●), <sup>15</sup>N<sub>2</sub>O (◆), Ar and Inverse Ar (□).

It is seen that the unlabelled N<sub>2</sub>O signal reaches a value of zero more rapidly than that of the unlabelled N<sub>2</sub> species. The same is true of the profile relating to the mixed-labelled N<sub>2</sub>O relative to the mixed-labelled N<sub>2</sub> profile. This is more clearly seen in Fig. 3, where the α profiles for N<sub>2</sub> (■) and N<sub>2</sub>O (●) are presented along with the profile for <sup>15</sup>NO (○) and <sup>15</sup>NO<sub>2</sub>

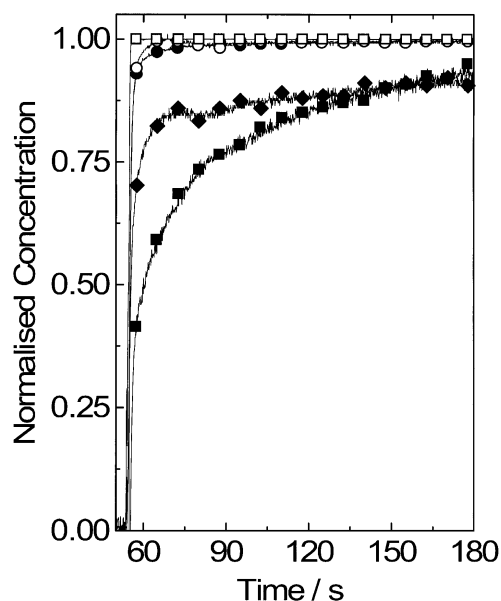


FIG. 3. The α N<sub>2</sub> (■), α N<sub>2</sub>O (●), <sup>15</sup>NO (○), <sup>15</sup>NO<sub>2</sub> (◆), and inverted Ar (□) profiles from the experiment shown in Fig. 2.

(◆). The  $\alpha$  function has previously been described as the fraction of reactant or product that is made up of labelled ( $^{15}\text{N}$ ) atoms following the  $^{14}\text{NO} \rightarrow ^{15}\text{NO}$  switch (21); i.e., in the case of  $\text{N}_2$ ,  $\alpha(\text{N}_2)$  is defined as

$$\alpha(\text{N}_2) = \frac{[^{15}\text{N}_2] + 0.5[^{15}\text{N}^{14}\text{N}]}{[^{15}\text{N}_2] + [^{14}\text{N}^{15}\text{N}] + [^{14}\text{N}_2]} \quad [1]$$

A similar function can be constructed for  $\alpha(\text{N}_2\text{O})$  while  $\alpha(\text{NO})$  and  $\alpha(\text{NO}_2)$  can be taken directly from the normalised  $^{15}\text{NO}$  and  $^{15}\text{NO}_2$  readings. It is seen that the  $\alpha(\text{N}_2\text{O})$  and  $\alpha(\text{NO})$  plots are, to a first approximation, the same as one another. This is a situation that has been seen before for the  $\text{NO}/\text{H}_2$  system (11) and shows that  $\text{N}_2\text{O}$  which contains an  $^{14}\text{N}$  atom can only continue to be formed for as long as there is  $^{14}\text{NO}$  in the system.

In contrast to this, when the  $\text{NO}/\text{C}_3\text{H}_6/\text{O}_2$  system (21) was studied over the same catalysts, below the temperature of hydrocarbon “light-off” it was found that there was no difference between the Ar profile and that of the  $^{15}\text{NO}$ . This indicated that there was no steady-state desorption of  $\text{NO}$  from the catalyst while it was operating in the case of the  $\text{NO}/\text{C}_3\text{H}_6/\text{O}_2$  reaction (below hydrocarbon “light-off”) but that such a desorption does take place in the case of the  $\text{NO}/\text{H}_2$  and  $\text{NO}/\text{H}_2/\text{O}_2$  reactions.

The  $\alpha(\text{N}_2)$  and  $\alpha(\text{NO}_2)$  profiles are very far removed from the Ar profile and are delayed for  $\sim 250$  s before reaching a normalised value of 1. In the case of the  $\text{N}_2$  product this is a situation that was also seen in the case of the  $\text{NO}/\text{H}_2$  reaction (11) and also the  $\text{NO}/\text{C}_3\text{H}_6/\text{O}_2$  reaction (21); i.e.,  $\text{N}_2\text{O}$ , was the isotopically first product and  $\text{N}_2$  was the isotopically second.

In the case of  $\text{NO}_2$  the situation is a little more complex. There was a delay in the removal of  $\text{NO}_2$  from the reactor following the  $^{14}\text{NO} \rightarrow ^{15}\text{NO}$  switch, and this delay was not associated with the catalyst as it was also present when quartz chips were used alone in the reactor *and* when the reactor was empty. The production of  $\text{NO}_2$  was rather small and *decreased* as the temperature was raised from 60 to  $83^\circ\text{C}$ , and thus the normalised plots of  $^{15}\text{NO}_2$  became very noisy (as the difference between normalised values of 0 and 1 are small). However, the order of the labelled molecules in the effluent always remained  $\text{NO} \approx \text{N}_2\text{O}$ , followed by  $\text{NO}_2$  followed by  $\text{N}_2$ .

From a standard SSITKA (14) the difference in area between the Ar profile and the various  $\alpha$  profiles can be used to obtain a value for the mean surface residence time ( $\tau$ ) for the species on the surface leading to products. For example, in the case of  $\text{N}_2$ ,

$$\tau(\text{N}_2) = \int_0^\infty \bar{\alpha}(\text{N}_2) dt, \quad [2]$$

where  $\bar{\alpha}$  represents the  $(1-\alpha)$  profile in the case of the  $^{14}\text{NO}$  to  $^{15}\text{NO}$  switch and the  $\alpha$  profile in the case of the

$^{15}\text{NO}$  to  $^{14}\text{NO}$  switch. The “mean surface residence times” ( $\tau$ ) of the species leading to products, as well as the rates of formation of the various products, are shown as a function of temperature in Table 1. It can be seen that the increase in temperature between 60 and  $83^\circ\text{C}$  resulted in a decrease in the mean surface residence times for  $\text{N}_2$  and  $\text{N}_2\text{O}$ .

These values ( $\tau$  and  $r$ ) can be used to yield values for the concentration of adsorbed surface species leading to product and of adsorbed reactant which simply desorbs. For example, in the case of  $\text{N}_2$  or  $\text{N}_2\text{O}$  this is calculated from the relationship

$$2 * \tau_{(\text{N}_2 \text{ or } \text{N}_2\text{O})} * r_{(\text{N}_2 \text{ or } \text{N}_2\text{O})} = N_{(\text{N}_2 \text{ or } \text{N}_2\text{O})}, \quad [3]$$

where  $\tau$  is the mean surface residence time (s),  $r$  is the rate of production of the product molecule ( $\mu\text{mol g}^{-1} \text{s}^{-1}$ ), and  $N$  is the concentration of active sites ( $\mu\text{mol g}^{-1}$ ). The number 2 represents the number of atoms of labelled element per molecule (2 in the case of  $\text{N}_2$  and  $\text{N}_2\text{O}$ , 1 in the case of  $\text{NO}$  and  $\text{NO}_2$ ). A more general method for calculating the surface concentrations of adsorbed intermediates using the  $\alpha$  functions has been proposed previously (21).

Table 2 shows the calculated concentration of sites on the surface as determined from this analysis at the two temperatures studied. It can be seen that the reason for the increase in the activity of the catalyst for the production of  $\text{N}_2$  is due to an increase in the concentration of sites ( $5.1 \rightarrow 7.6 \mu\text{mol g}^{-1}$ ) active for the production of  $\text{N}_2$  and to an increase in the overall “reactivity” of these sites (as qualitatively measured by the reciprocal of the mean surface residence time, which decreases from 64 to 42 s). It should be remembered that this is a qualitative measurement only and only truly holds for unidirectional first-order reactions.

The increase in the production of  $\text{N}_2\text{O}$  is *more* due to an increase in the concentration of sites ( $1 \rightarrow 1.8 \mu\text{mol g}^{-1}$ ) active for its production although the “activity” of the sites also increases somewhat ( $1.1 \rightarrow 0.7$  s). The determination of the increase in the activity and concentrations of the sites that produce  $\text{N}_2\text{O}$  is heavily influenced by errors in the calculation of  $\tau$  (estimated as 0.5) while such errors are less influential in the case of the production of  $\text{N}_2$ —as its residence time is considerably higher.

TABLE 2

Concentrations of Adsorbed Species  $N$  ( $\mu\text{mol g}^{-1}$ ) on the Surface of 5% Pt/SiO<sub>2</sub> as a Function of Temperature during the  $\text{NO}/\text{H}_2/\text{O}_2$  Reaction as Measured by SSITKA Analysis

	$N(\text{N}_2)$	$N(\text{N}_2\text{O})$	$N(\text{NO})$	$\sum N$
60	$5.1 \pm 0.04$	$1.0 \pm 0.5$	$6.0 \pm 5$	$12.1 \pm 5.5$
83	$7.6 \pm 0.1$	$1.8 \pm 1.3$	$6.8 \pm 4.3$	$16.2 \pm 5.7$

Note. The reactant stream contained 1.64%  $\text{NO}$ , 1.64%  $\text{H}_2$ , and 8.7%  $\text{O}_2$  with an He carrier gas in a total flow of  $113 \text{ cm}^3 \text{ min}^{-1}$  over a 5% Pt/SiO<sub>2</sub> catalyst (0.113 g).

TABLE 3

Coverages of Surface Intermediates  $\Theta$  ( $\times 100$ ) on 5% Pt/SiO<sub>2</sub> as a Function of Temperature during the NO/H<sub>2</sub>/O<sub>2</sub> Reaction as Measured by SSITK Analysis

	$\Theta(\text{N}_2)$	$\Theta(\text{N}_2\text{O})$	$\Theta(\text{NO})$	$\Theta$
60	6 $\pm$ 0.1	1 $\pm$ 0.6	8 $\pm$ 6.4	16 $\pm$ 7.1
83	10 $\pm$ 0.1	2 $\pm$ 1.6	9 $\pm$ 5.4	20 $\pm$ 7.1

*Note.* The reactant stream contained 1.64% NO, 1.64% H<sub>2</sub>, and 8.7% O<sub>2</sub> with an He carrier gas in a total flow of 113 cm<sup>3</sup> min<sup>-1</sup> over a 5% Pt/SiO<sub>2</sub> catalyst (0.113 g). The Pt catalyst had  $4.74 \times 10^{19}$  Pt atoms exposed to the gas phase.

The concentration of adsorbed species can be related to the metal surface area of the Pt. Table 3 shows the metal surface coverage of species leading to N<sub>2</sub> and N<sub>2</sub>O as well as the surface coverage of adsorbed unreacted NO as a function of temperature during the NO/H<sub>2</sub>/O<sub>2</sub> reaction. It is seen that the calculated surface coverages of N<sub>2</sub> and N<sub>2</sub>O precursors on the surface are 6 and 1%, respectively, at 60°C, and these values increase to  $\sim 10$  and  $\sim 2\%$ , respectively, as the temperature is raised to 83°C. Note again that the errors in the calculation of the  $\tau(\text{N}_2\text{O})$  value result in substantial errors in the calculation of the  $\text{N}(\text{N}_2\text{O})$  value and thus in the  $\Theta(\text{N}_2\text{O})$  value. However, even taking these substantial errors into account the surface coverage of intermediates which go on to form N<sub>2</sub>O is far lower than that of intermediates which go on to form N<sub>2</sub>.

The coverages of unreacting NO, which is also heavily influenced by possible error in the calculation of  $\tau(\text{NO})$ , remains rather constant between the two temperatures. The overall surface coverage of NO-derived species increases from  $\sim 16$  to  $\sim 20\%$ , showing that the surface of the Pt is never fully covered with N-containing species that either desorb or go on to form products. Even at the upper limit of the possible NO-derived surface coverage ( $\sim 27\%$ ) most of the Pt sites are not covered with species that (a) form N<sub>2</sub>, (b) form N<sub>2</sub>O, or (c) desorb as unreacted NO.

The remainder of the surface could be covered with H<sub>2</sub>- or O<sub>2</sub>-derived species or covered by NO-derived spectator species that are stable under these conditions. It is known (35) from TPD experiments that NO<sub>2,ads</sub>-type species can form on Pt and that these species are relatively stable at the temperatures used here.

## DISCUSSION

There are similarities between the results presented here and those seen before in the analysis of the NO/C<sub>3</sub>H<sub>6</sub>/O<sub>2</sub> (21) and NO/H<sub>2</sub> (11) reactions. On a quantitative level it is again seen that the reason for the increase in the production of N<sub>2</sub> with temperature is due to an increase in the concentration and activity of sites which produce N<sub>2</sub>. The

increase in production of N<sub>2</sub>O with temperature is *more* due to an increase in the concentration of sites which produce N<sub>2</sub>O than to an increase in their activity. The production of N<sub>2</sub>O requires the presence of some reversibly adsorbed NO molecules to proceed. The isotopic order of production of the product molecules (N<sub>2</sub> and N<sub>2</sub>O), following the switch, is again the same, with N<sub>2</sub>O being isotopically first and N<sub>2</sub> being isotopically last. This leads to the exclusion of several mechanisms and must lead to the development of a mechanism in which N<sub>2</sub>O is produced from earlier intermediates in a reaction sequence than those that produce N<sub>2</sub> (21).

In order to provide a more detailed mechanism for the reaction, we shall use three different analyses (and transformations) of the experimental profiles for the NO + H<sub>2</sub> reaction in relation to the information they yield about the N<sub>2</sub> and N<sub>2</sub>O forming reactions. These analyses are: (a) the Initial Distribution of Isotopic Molecules of Product (IDIMP), which gives some information about the possibilities of there being more than one route to the formation of various products; (b) the Temporal Redistribution of the Isotopic Molecules of Product, (TRIMP), which gives information about the nature of the final intermediates on the surface before the final act of production of the doubly labelled product molecule; and (c) a semilogarithmic plot of the  $\bar{\alpha}$  function versus time (where  $\alpha$  is the fraction of heavy atoms in the gas phase), which tells of the presence of buffer states, consecutive, parallel routes, etc.

IDIMP is a "snapshot" of the initial redistribution immediately following a <sup>14</sup>NO + H<sub>2</sub>  $\rightarrow$  <sup>15</sup>NO + H<sub>2</sub> switch, while TRIMP and the semilogarithmic plot are presented as functions of time. It should be noted that IDIMP has been used previously for studying reactions such as benzene hydrogenation in flow systems (36, 37). The TRIMP plots relate to isotopic equilibrium, a concept which has been previously studied in isotopic exchange reactions (see below), although never in terms of SSITKA. The first two sets of profiles, (a) and (b), are discussed in terms of the concept of "Types of Production" of two-atom labelled molecules (PA<sub>2</sub>). The IDIMP plots are also used to introduce the concept of the integral characteristics of any network mechanism of the form RA<sub>n</sub>  $\rightarrow$  ... IA<sub>x</sub> ...  $\rightarrow$  PA<sub>2</sub>, i.e., where a labelled reactant (RA<sub>n</sub>) progresses through one or more surface intermediates (IA<sub>x</sub>) to yield a two-atom labelled molecule (PA<sub>2</sub>). Full details can be found elsewhere (34), but the main features of these analyses are described below.

## TYPES OF PRODUCTION OF TWO-ATOM LABELLED MOLECULES

In order to discuss the first and second transformations (IDIMP and TRIMP) of the data we introduce the concept of "Types of Production." This involves discriminating between alternative steady-state reaction mechanisms on the basis of the *final* reaction step leading to the generation

TABLE 4

The Five Possible Types of Production of a Product Molecule PA<sub>2</sub> from a Reactant Molecule RA and Reaction Intermediates (IA and I'A) and the Final Reaction Steps

Type of production	Mechanism of final step	Temporal redistribution $y_i = x_i - x_i^{\text{eq}}$	Initial distribution $\{x_0^0, x_1^0, x_2^0\}$	Production coefficient $C_{\text{PR}}$	Percolation coefficient $C_{\text{PE}}$
0	2RA → PA <sub>2</sub>	$y_1 = y_2 = 0$	{0, 0, 1}	0	2
1	RA + IA → PA <sub>2</sub>	$y_1 > 0, y_2 < 0$	{0, 1, 0}	1	1
2a	2IA → PA <sub>2</sub>	$y_1 = y_2 = 0$	{1, 0, 0}	2	0
2b	IA + I'A → PA <sub>2</sub>	$y_1 > 0, y_2 < 0$	{1, 0, 0}	2	0
2c	IA <sub>2</sub> → PA <sub>2</sub>	$y_1 < 0, y_2 > 0$	{1, 0, 0}	2	0

Note. Also shown are the predicted deviations of the fraction of isotopic molecules (PA<sub>2-*i* A<sub>i</sub>) from equilibrium ( $x_i^{\text{eq}}$ ) of the isotopically labelled molecules ( $y_1$  P\*AA and  $y_2$  PA\*A\*), the expected initial isotopic distribution following the same switch, and the expected production ( $C_{\text{PR}}$ ) and percolation ( $C_{\text{PE}}$ ) coefficients following a step change RA → RA\*.</sub>

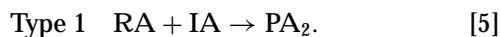
of the product molecule (PA<sub>2</sub>) from the reactant (RA<sub>*n*</sub>) and any final intermediates on the surface (IA<sub>*x*</sub> or I'A<sub>*x*</sub>).

Detailed analysis (34) of the modes of production of a molecule of product (PA<sub>2</sub>) containing two “labellable” A atoms from a labelled reactant molecule (RA<sub>*n*</sub>) and intermediates IA<sub>*x*</sub> has shown that there are basically five “pure” Types of Production of such molecules. These are shown in Table 4 and are briefly discussed below. In the following presentation, “A” represents a labelled atom (with two possible isotopes), RA<sub>*n*</sub> represents a reactant containing “*n*” such atoms, PA<sub>2</sub> represents a product containing two such A atoms, and IA<sub>*x*</sub> represents an intermediate containing “*x*” A atoms. R, P, and I are parts of the molecule that do not contain any A atoms (or contain A atoms that remain unreactive). We will consider a singly labelled reactant (RA) and either singly or doubly labelled intermediates, i.e.,  $x=1$  or 2 (IA and IA<sub>2</sub>), to simplify the types of production that we will discuss.

The first type of production (labelled 0) is one in which the surface plays no measurable role and the production of PA<sub>2</sub> involves no surface A atoms, i.e.,



The second type (labelled 1) involves, for example, an impact mechanism in which a molecule of RA interacts with a surface intermediate. Each of these species yields one A atom to produce a PA<sub>2</sub> molecule. This involves one surface A atom in the elementary act of production of PA<sub>2</sub>, i.e.,

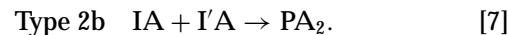


The third, fourth, and fifth methods of formation of PA<sub>2</sub> all involve two surface A atoms in the final act of production. These are labelled “2” and are differentiated on the basis of different types of final interactions. Production type 2a (a for alone) represents the formation of a PA<sub>2</sub> molecule from two equivalent moieties on the surface, both

of which give one A atom to the final product, i.e.,



Production type 2b (b for binary) represents the formation of PA<sub>2</sub> from the interaction of two *different* surface species, both of which give 1 A atom to the final product, i.e.,



The final type of production of PA<sub>2</sub> is type 2c (c for coupled), and this involves the presence of a “coupled” intermediate on the surface which contains, as a minimum, two A atoms. In this case both atoms that go on to form PA<sub>2</sub> originate from the same species, i.e.,



These different types of production lead to different responses in the first and second features of the obtained profiles, i.e., Initial Distribution of Isotopic Molecules of Product (IDIMP) and Temporal Redistribution of Isotopic Molecules of Product (TRIMP). The expected outcomes of these transformations from any “pure” type of production (0, 1, 2a, 2b, or 2c) are detailed in Table 4. It must be remembered that these formalisms do not necessarily represent actual reactions but rather just “modes” of reaction and that the action of any type can lead to different profiles which depend on factors such as surface concentrations, rates, and reversibility of steps. However, qualitatively the temporal redistribution profiles and the initial distribution plots developed for each type of production must have the same individual features.

It must also be noted that for a particular “Type of Production” the atomicity of the surface intermediates (IA<sub>*x*</sub>) is unimportant and the individual features of IDIMP and the qualitative features of TRIMP will remain the same; e.g., IA<sub>2</sub> + I'A<sub>2</sub> → PA<sub>2</sub> + IA + I'A also represents a type 2b production and IA<sub>3</sub> → PA<sub>2</sub> + IA represents type 2c production, and both will give the corresponding IDIMP and qualitative TRIMP features. Isotopic exchange of the product

molecules (through adsorption/desorption processes) with either the final intermediates or with different sites on the surface must also be allowed for. In these cases the situation becomes more complex and these will not be considered further here (see (34)). However, for many experimental cases regarding molecules such as N<sub>2</sub> and N<sub>2</sub>O, these exchange reactions are not important.

In terms of the Types of Production we can also say that the overall rate of production of the two-atom molecule (PA<sub>2</sub>) equals the sum of the individual rates of the five types of production (in a normalised form at a value of 1),

$$\chi_0 + \chi_1 + \chi_{2a} + \chi_{2b} + \chi_{2c} = 1 \quad [9]$$

where  $\chi_k$  represents the contribution of type  $k$  ( $k=0, 1, 2a, 2b, 2c$ ), with a rate  $R_k$ , in the overall production (with a rate  $R_\Sigma$ ), and therefore  $\chi_k = R_k/R_\Sigma$ . The strict method of calculating  $\chi_k$  on the basis of isotopic kinetic equations will be presented elsewhere (34). A second, simpler, but less accurate method based on IDIMP will be discussed below.

#### a. Initial Distribution of Isotopic Molecules of Product (IDIMP)

If we consider the overall production of an isotopic product molecule containing two "labellable" atoms following the RA + ( ) → \*RA + ( ) switch within the SSITKA, there are normalised connections for the Initial Distribution of the Isotopic Molecules of Product; e.g.,

$$x_0^0 + x_1^0 + x_2^0 = 1 \quad [10]$$

(where  $x_i^0$  represents the initial fraction of isotopic molecules which contain  $i$  heavy atoms, e.g., <sup>14</sup>N<sub>2- $i$</sub> <sup>15</sup>N <sub>$i$</sub> ). Overall, the production of N<sub>2</sub> remains constant, and therefore, the sum of the fractions of all isotopic molecules must, at all times, equal a normalised value of 1.

The initial isotopic product distribution following the RA + ( ) → R\*A + ( ) switch (in our case <sup>14</sup>NO + O<sub>2</sub> + H<sub>2</sub> → <sup>15</sup>NO + O<sub>2</sub> + H<sub>2</sub>) is different for some of the types of production of PA<sub>2</sub> detailed above. Type 0 results in the initial distribution being fully doubly labelled, while type 1 production leads to fully singly labelled, and all type 2 productions (2a, 2b and 2c) lead to unlabelled product molecules in the initial isotopic distribution (see Table 4).

The initial isotopic distribution and the contributions of the different types of production can be related. If the probability (or contribution) of type of production  $k$  is  $\chi_k$  and the initial isotopic distribution is represented as  $\{x_0^0, x_1^0, x_2^0\}$ , then it can be shown that

$$x_0^0 = \chi_{2a} + \chi_{2b} + \chi_{2c} \quad [11]$$

$$x_1^0 = \chi_1 \quad [12]$$

$$x_2^0 = \chi_0. \quad [13]$$

That is to say, the initial distribution gives direct information about the contributions of various types of production to the overall production of PA<sub>2</sub>.

These are obviously theoretical calculations, and it can be shown (34) that the imposition of an experimental switch rather than an ideal switch from RA to R\*A does change this distribution somewhat. In the specific case of the NO + O<sub>2</sub> + H<sub>2</sub> reaction over Pt/SiO<sub>2</sub> this makes any IDIMP analysis of the N<sub>2</sub>O distribution more prone to errors as this is very rapid relative to the N<sub>2</sub> redistribution and thus more prone to effects of the imposed "experimental" switch. Generally then, with respect to the gaseous holdup of the system, the "shorter" the holdup the more accurate the IDIMP.

Plots of the IDIMP are constructed by taking the normalised values for all the isotopic molecules of N<sub>2</sub>O and N<sub>2</sub> at a short time following the switch. Obviously for experimental reasons it is not possible to get readings directly after the switch (due to perturbations in the gas stream), and thus readings are taken ~3 s after the beginning of the switch. At this time the Ar has reached a normalised value of 1, the mixed-labelled products (<sup>14</sup>N<sup>15</sup>N and <sup>14</sup>N<sup>15</sup>NO) are at maxima, and the product redistribution is in process. Taking the readings as these mixed species are at their maxima can most accurately compensate for the "experimental nature" of the switch (and its effects on the accuracy of the IDIMP analysis).

Figure 4 shows this analysis for the N<sub>2</sub> and the N<sub>2</sub>O products formed following the <sup>14</sup>NO/O<sub>2</sub>/H<sub>2</sub> → <sup>15</sup>NO/O<sub>2</sub>/H<sub>2</sub> switch at 70°C. The results are presented as bar charts showing the normalised production on the ordinate and the

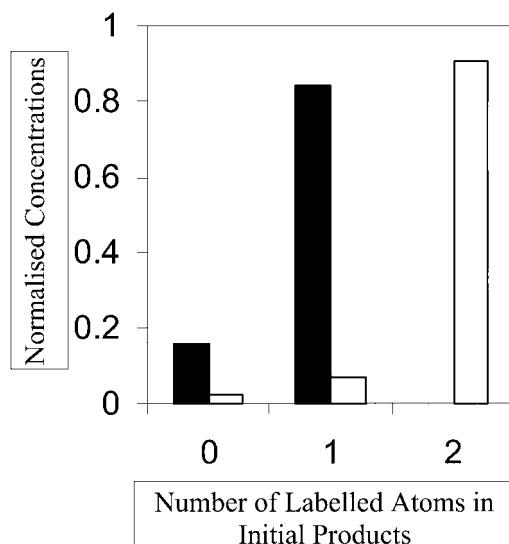


FIG. 4. IDIMP analysis of the isotopic products of the NO/O<sub>2</sub>/H<sub>2</sub> → <sup>15</sup>NO/O<sub>2</sub>/H<sub>2</sub> switch over 5% Pt/SiO<sub>2</sub> at 70°C. N<sub>2</sub> ■, N<sub>2</sub>O □. (2.5% NO and H<sub>2</sub>, 14% O<sub>2</sub> and He balance, to 73 cm<sup>3</sup> min<sup>-1</sup> over 113 mg 5% Pt/SiO<sub>2</sub>.)

number of labelled atoms on the abscissa. Most of the  $N_2O$  molecules formed at this stage are doubly labelled. From the analysis presented in Table 4, this indicates a very high level of type 0 production. However, it must be remembered that the accuracy of this is very questionable due to the rapid nature of the transient with respect to the  $N_2O$  formation.

A more interesting and informative situation is seen in the case of the  $N_2$  IDIMP results. Here the initial distribution can be written as  $\{x_0^0, x_1^0, x_2^0\} = \{0.15 \pm 0.05, 0.85 \pm 0.05, 0\}$ . This can be compared to the results for the  $N_2$  IDIMP from the  $NO/H_2$  reaction (11), i.e.,  $\{0.3 \pm 0.05, 0.7 \pm 0.05, 0\}$ . It can be seen that the initial fraction of the doubly labelled product is unchanged but that the mixed-labelled species is now more prominent ( $0.7 \rightarrow 0.85$ ) and the unlabelled species is less prominent ( $0.3 \rightarrow 0.15$ ). In terms of the contributions of various "types of production," this indicates

$$x_0^0 = \chi_{2a} + \chi_{2b} + \chi_{2c} = 0.15 \quad [14]$$

$$x_1^0 = \chi_1 = 0.85 \quad [15]$$

$$x_2^0 = \chi_0 = 0. \quad [16]$$

where  $\chi_n$  represents the contribution of type of production  $n$  ( $n = 0, 1, 2a, 2b, 2c$ ).

This shows that a type 1 production operates here (as this produces the initial amount of  $^{14}N^{15}N$ ) as does some type 2 (a, b, or c), as this leads to the unlabelled product. Also the contribution of the "type 1" reaction is increased relative to that of some "type 2 (a, b, c)" mechanism when this reaction ( $NO/O_2/H_2$ ) is compared to the  $NO/H_2$  reaction under the same conditions.

We now reintroduce (11, 34) two integral characteristics which reflect the degrees of surface intermediate (or lattice) participation in the formation of doubly labelled product molecules ( $PA_2$ ) from labelled molecules ( $RA_n$ ) and their connection with the above-mentioned "Initial Distribution of Isotopic Molecules of Product."

First is the Coefficient of Surface Production ( $C_{PR}$ )—this is the average number of surface A atoms which participate in one act of production (desorption) of a molecule  $PA_2$ . Second is the Coefficient of Percolation ( $C_{PE}$ ), which is the average number of A atoms of the reactant RA which participate in one elementary act of formation of the product molecule  $PA_2$ .

In the production of the molecule  $PA_2$  there is the obvious relationship

$$C_{PR} + C_{PE} = 2. \quad [17]$$

With regard to the five types of production the Percolation and Surface Production Coefficients for each type of production are presented in Table 4. These are derived using

IDIMP and the simple equations

$$C_{PR} = 2x_0^0 + x_1^0 \quad [18]$$

$$C_{PE} = x_1^0 + 2x_2^0. \quad [19]$$

Here the values  $x_0^0, x_1^0$ , and  $x_2^0$  represent the initial normalised fractions of the fully unlabelled, mixed labelled, and fully labelled initial product species, respectively.

In the present case (the  $NO/O_2/H_2$  reaction over 5% Pt/SiO<sub>2</sub> at 70°C under steady-state conditions) for  $N_2$  the  $C_{PR} = 1.15$  and the  $C_{PE} = 0.85$ . This simply means that every molecule of  $N_2$  produced takes an average of 1.15 N atoms from the surface and an average of 0.85 atoms from the gas phase. This compares with values of  $C_{PR} = 1.3$  and  $C_{PE} = 0.7$  from the  $NO/H_2$  reaction over the same catalysts and reflects the decreased contribution of the "type 2 (a, b or c)" process for the formation of  $N_2$  in this reaction. It is not feasible to carry out this analysis for the  $N_2O$  production since the switch is too fast.

### b. Temporal Redistribution of Isotopically Labelled Molecules of Product (TRIMP)

An important characteristic of isotopically labelled molecules with more than one labelled atom of the same element is the amount of the redistribution of the isotopic equilibrium present. This is the situation in our case regarding the product molecules ( $N_2$  and  $N_2O$ ). If these molecules are in a state of isotopic equilibrium, then when the fraction of heavy isotopes ( $^{15}N$ ) in the gas phase is  $\alpha$ , the equilibrium fraction ( $x_i^{eq}$ ) of the isotopic molecules, e.g.,  $^{15}N_i^{14}N_{(2-i)}$ , can be calculated using the binomial distribution (28, 31)

$$x_i^{eq} = \binom{2}{i} \alpha^i (1 - \alpha)^{2-i}, \quad [20]$$

where

$$\binom{2}{i} = \frac{2!}{(2-i)!i!} \quad \text{for } i = 0, 1, 2. \quad [21]$$

A useful probe function for the extent of isotopic equilibrium in an flow system is the deviation ( $y_i$ ) of the fraction of isotopic molecules  $^{14}N_{(2-i)}^{15}N_i$  ( $x_i$ ) from their equilibrium fraction  $x_i^{eq}$ . This function was first used by Muzykantov *et al.* (28) in the analysis of isotopic exchange of  $O_2$  in a closed system.

$$y_i = x_i - x_i^{eq} \quad \text{for } i = 0, 1, 2. \quad [22]$$

For the  $^{14}N^{15}N$  molecule, which contains one heavy atom,

$$y_1 = x_1 - 2\alpha(1 - \alpha). \quad [23]$$

When the isotopic molecules  $PA_{2-i}^*A_i$  are statistically mixed, then  $y_i = 0$  for  $i = 0, 1, 2$ . TRIMP shows the  $y_i$  variable for the isotopic molecules of product as a function of



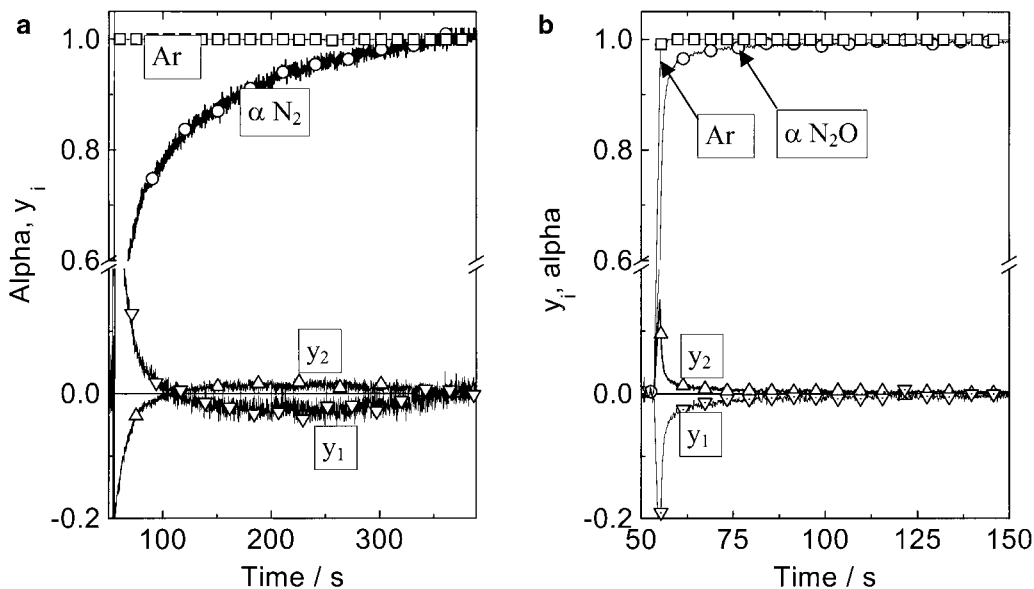


FIG. 5. TRIMP plots (in the  $y_i$ -time coordinate) for (a)  $^{15}\text{N}_2$  ( $y_2$ ) ( $\Delta$ ) and  $^{14}\text{N}^{15}\text{N}$  ( $y_1$ ) ( $\nabla$ ) and for (b)  $^{15}\text{N}_2\text{O}$  ( $y_2$ ) ( $\Delta$ ) and  $^{14}\text{N}^{15}\text{NO}$  (and  $^{15}\text{N}^{14}\text{NO}$ ) ( $y_1$ ) ( $\nabla$ ) following the same experiment shown in Fig. 4. Profiles for the respective  $\alpha$  function ( $\circ$ ) and the inverted Ar trace ( $\square$ ) are also shown.

time following an isotopic step change, e.g., in our case the  $^{14}\text{NO}/\text{O}_2/\text{H}_2 \rightarrow ^{15}\text{NO}/\text{O}_2/\text{H}_2$  switches.

For a complete description of the composition of isotopic molecules, e.g.,  $\text{PA}_2-i^*A_i$ , we only need to examine one isotopic species, i.e., ( $\text{PA}_2$ ,  $\text{PA}^*A$ , or  $\text{P}^*A_2$ ), in conjunction with the  $\alpha$  profile. This is because the three deviations from equilibrium ( $y_0$ ,  $y_1$ , and  $y_2$ ) are related (at any time ( $t$ )) by the relationships

$$y_0(t) + y_1(t) + y_2(t) \equiv 0, \quad y_0(t) \equiv y_2(t), \quad \text{and} \\ y_1(t) \equiv -2^*y_0(t) \text{ (or } -2^*y_2(t)). \quad [24]$$

This indicates that the largest deviation from equilibrium will be seen for the  $y_1(t)$  profile (representing the deviation from equilibrium for the  $^{14}\text{N}^{15}\text{N}$  species) and that the  $y_2(t)$  and  $y_0(t)$  profiles (which represent the deviations for the  $^{14}\text{N}^{14}\text{N}$  and the  $^{15}\text{N}^{15}\text{N}$  species) will be mirror images of this profile but will be one half as intense. In this work we show both the  $y_1(t)$  and the  $y_2(t)$  profiles along with the  $\alpha$  profile.

Table 4 shows how any variation in the “Type of Production” is manifested in a change in the TRIMP profiles for a plug flow reactor. For types 0 and 2a the isotopic molecules of product are always statistically mixed; i.e.,  $y_1 = y_2 = 0$ . For types 1 and 2b there is superproduction of the mixed-labelled species for a time following the switch; i.e.,  $y_1 > 0 > y_2$ . Conversely, for type 2c there is subproduction of the mixed-labelled species for a time following the switch; i.e.,  $y_1 < 0 < y_2$ . These only apply in the case of “pure” types of production, and any concurrent operation of more than one type of production will lead to situations that are more complex. The operation of more than one “type” (for multiroute mechanisms) does *not* gener-

ally yield a simple profile resulting from the average of the profiles of the types involved.

The imposition of an experimental step change rather than an ideal one also causes some deviation from “true”  $y_i$  profiles in this analysis. This deviation is only seen at the beginning of the switch when the inverted Ar profile has not reached a steady value (0 in our case as  $^{14}\text{NO}/\text{Ar}$  is removed from the stream). The TRIMP profiles for the  $^{14}\text{NO}/\text{O}_2/\text{H}_2 \rightarrow ^{15}\text{NO}/\text{O}_2/\text{H}_2$  switch are shown in Figs. 5a ( $\text{N}_2$ ) and 5b ( $\text{N}_2\text{O}$ ).

It can be seen that in both cases the product molecules are not in isotopic equilibrium through the course of the switch. In the case of  $\text{N}_2\text{O}$  (Fig. 5b) there is an underproduction of the mixed-labelled  $^{14}\text{N}^{15}\text{NO}$  following the switch  $y_1 < 0$ , and this remains the situation until the  $\alpha(\text{N}_2\text{O})$  profile reaches 1. Correspondingly, there is an overproduction of the unlabelled and doubly labelled species until the  $\alpha(\text{N}_2\text{O})$  profile reaches 1. This is ascribed to the action of a “type 2c” mechanism in which the production of  $\text{N}_2\text{O}$  is through a coupled intermediate and is similar to the situation seen for  $\text{N}_2\text{O}$  production in the  $\text{NO}/\text{H}_2$  reaction (11). This is in contrast to the IDIMP results, which indicate the action of a “type 0” mode, but it must be remembered that the IDIMP analysis is far more sensitive to the rapid nature of the switch than is the TRIMP analysis.

In the case of the TRIMP profiles for  $\text{N}_2$  production there is an overproduction of  $^{14}\text{N}^{15}\text{N}$  directly following the switch, but this turns into an underproduction  $\sim 60$  s after the switch. There are two situations in which this profile can be expected. In both situations there are two routes to  $\text{N}_2$  formation, and these operate in an “isotopically first” and an “isotopically second” type of order.

The first of these situations involves the interaction of a “type 1” impact mechanism, where gas-phase or physisorbed NO interacts with an N-containing species on the surface to form  $N_2$  (leading to the overproduction of  $^{14}N^{15}N$ ), and a “type 2a” mechanism, where two identical species on the surface interact to give  $N_2$  (which in this case leads to an underproduction of  $^{14}N^{15}N$ ). This is interesting because a pure 2a type of production yields no deviation from equilibrium but a “type 2a” in combination with a “type 1” (1 + 2a) yields this type of profile (as has been discussed in more detail previously (11)).

The second situation in which the interaction of two types of production can lead to this TRIMP profile involves a “type 1” impact mechanism (as above) in conjunction with a “type 2c” production, where the final reaction step involves a species on the surface which gives two N atoms to the  $N_2$  molecule (coupled intermediate) (1 + 2c).

Previously (11), the  $y_i$  profiles (in the  $\alpha$  coordinate) were used to distinguish between production via the operation of a 1 + 2a combination and that via a 1 + 2c combination. The basis of this discrimination centered around the fact that in the former case the  $y_1$  (and  $y_2$ ) profiles returned to 0 before the  $\alpha$  value reached 1. However, in the latter case this was not what modelling predicted; i.e.,  $y_1$  remains negative until  $\alpha$  becomes 1. In this case the data are a lot noisier than was seen in the NO/ $H_2$  case, but it is still clear (Fig. 6) that  $y_1$  and  $y_2$  reach values of 0 before the  $\alpha$  value reaches 1. Thus we can rule out a 1 + 2c mechanism in favour of a 1 + 2a one. This is a similar situation to that which was seen for the production of  $N_2$  in the NO/ $H_2$  reaction over Pt/ $SiO_2$ .

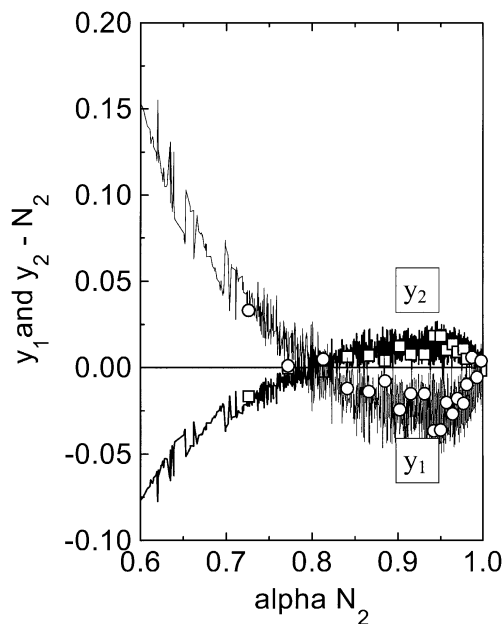


FIG. 6. The data presented in Fig. 5b presented in the  $y_i$ - $\alpha$  coordinate,  $y_1$  (○) and  $y_2$  (□).

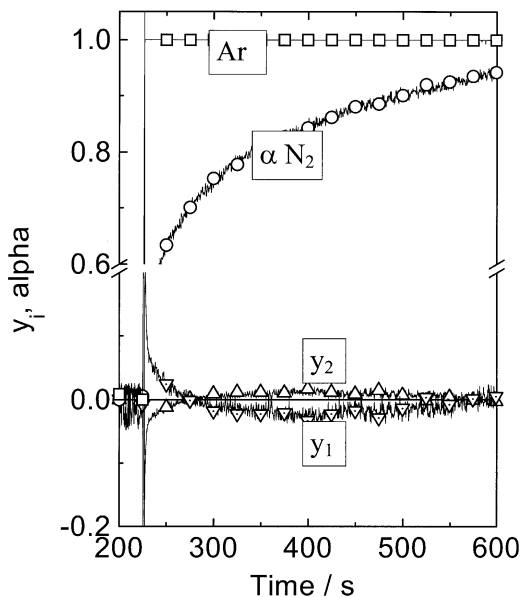


FIG. 7. TRIMP plots (in the  $y_i$ -time coordinate) for  $^{15}N_2$  ( $y_2$ ) (△) and  $^{14}N^{15}N$  ( $y_1$ ) (▽) following the  $^{14}NO/H_2 \rightarrow ^{15}NO/H_2$  switch at 70°C over 5% Pt/ $SiO_2$  (shown for reference from (11)). Profiles for the respective  $\alpha$  function (○) and the inverted Ar trace (□) are also shown.

Another feature of the profile which is similar to the ones taken from the NO +  $H_2$  reaction is the magnitude of the underproduction of the  $^{14}N^{15}N$  species. This never goes below  $\sim -3\%$ , indicating that the contribution of this 2a process, and thus the surface concentration of the final intermediates leading to  $N_2$  via type 2a, is not very large (as we surmised from the IDIMP results).

One quantitative difference between this result and that seen in the NO/ $H_2$  reaction is the larger magnitude of the overproduction of  $^{14}N^{15}N$  directly following the switch, e.g., when  $\alpha(N_2) = 0.6$  for both reactions following the  $^{14}NO \rightarrow ^{15}NO$  switch,  $y_1 = 0.04$  in the case of the NO/ $H_2$  reaction (Fig. 7) and  $y_1 = 0.15$  in the case of the NO/ $O_2$ / $H_2$  reaction (Fig. 5a). This indicates the increased contribution of type 1 to the formation of  $N_2$ . It is also noticeable that the switch is completed faster, i.e.,  $\alpha(N_2) = 1$ , in a shorter time following the switch in the presence of  $O_2$  (Fig. 5a) than in its absence (Fig. 7; Ref. (11)). This also qualitatively indicates the decreased contribution of the “type 2” process since it is this which is “isotopically second” in the production of  $N_2$ .

### c. Semilogarithmic Plots of the $\bar{\alpha}$ Function versus Time

The semilogarithmic plots of the  $\bar{\alpha}$  function versus time (11, 38) involve plotting the function  $|\ln|\bar{\alpha}||$  (where  $\bar{\alpha}$  represents the  $(1-\alpha)$  profile in the case of a  $^{14}NO \rightarrow ^{15}NO$  switch and the  $\alpha$  profile in the case of the reverse  $^{15}NO \rightarrow ^{14}NO$  switch) against time. The generated profiles give information about the reaction pathways leading to products. In this case  $\bar{\alpha}$  refers to  $1-\alpha$  as the switch considered is  $NO + (H_2/O_2) \rightarrow ^*NO + (H_2/O_2)$ . This presentation

is derived from classical isotopic exchange analysis and is used to reflect the heterogeneity of the surface (or lattice) intermediates.

Specifically, at steady state, this presentation gives information regarding the presence of a buffer step (in which a pool of inactive intermediates could be formed, in a reversible process, from a pool of active intermediates) or the presence of a consecutive mechanism (in which one pool of intermediates goes on to form another pool of intermediates before forming a product molecule), or, for example, the presence of a mechanism in which there is only one intermediate.

In each case the semilogarithmic plot of the  $\bar{\alpha}$  function versus time has a different shape. For the buffer step (first case) the curve is convex; in the consecutive mechanism (second case) it is concave; in the third case a straight line is obtained. A mechanism in which there are parallel routes leading to product and both show reversibility also yields a convex plot. Details of these different possibilities can be found in Table 5. The following shapes are expected. In the case of irreversible adsorption of reactant and desorption of product then, for a one-pool mechanism  $\alpha(t)$  is a function of one exponent (24) (therefore the semilogarithmic plot of the  $\bar{\alpha}$  function versus time is linear). Buffer (24) and parallel (14) pools result in  $\alpha(t)$  being the sum of two exponents (the semilogarithmic plot of the  $\bar{\alpha}$  function versus time is convex), and in the case of consecutive pools then  $\alpha(t)$  is the difference of two exponents (24) (the semilogarithmic plot of the  $\bar{\alpha}$  function versus time is concave). Combinations of these mechanisms lead to semilogarithmic plots of the  $\bar{\alpha}$  function versus time that are superpositions of the former plots.

Our results are generated from modelling reversible cases of adsorption of RA and desorption of PA<sub>2</sub> (when  $\alpha(t)$  cannot be represented in exponential form), and these show qualitatively similar shaped features to the situations

TABLE 5

Variations Expected in the Semilogarithmic Plots of the Function  $|\ln(\bar{\alpha})|$  against Time for Various Mechanisms for the Transformation of Reactant *R* into Product *P*

Label	Network mechanism	Shape of semilogarithmic plot (with time) $ \ln(\bar{\alpha}(t)) $
Direct	$R \rightleftharpoons I_1 \rightleftharpoons P$	straight line
Consecutive	$R \rightleftharpoons I_1 \rightleftharpoons I_2 \rightleftharpoons P$	concave curve
Buffer	$R \rightleftharpoons I_1 \rightleftharpoons P$ $\updownarrow$ $I_2$	convex curve
Parallel	$R \rightleftharpoons I_1 \rightleftharpoons P$ $R \rightleftharpoons I_2 \rightleftharpoons P$	convex curve

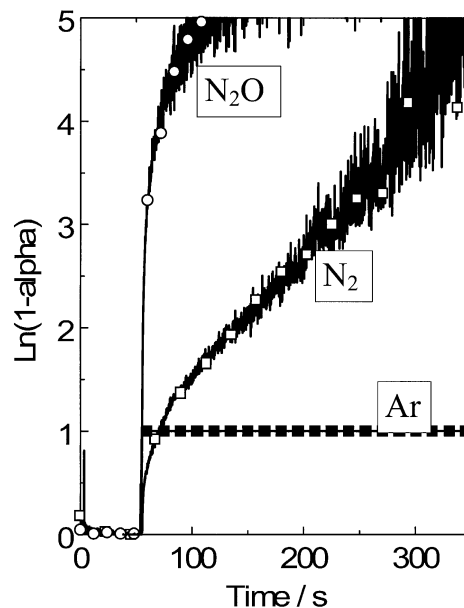


FIG. 8. Semilogarithmic plots of the function  $|\ln(\alpha)|$  against time for the product molecules N<sub>2</sub>O and N<sub>2</sub>, as well as an Ar profile following the <sup>14</sup>NO/H<sub>2</sub>/O<sub>2</sub> → <sup>15</sup>NO/H<sub>2</sub>/O<sub>2</sub> switch over 5% Pt/SiO<sub>2</sub> at 70°C. N<sub>2</sub> (□), N<sub>2</sub>O (○), inverted Ar (■).

discussed above. In the case of reversible adsorption of reactant, a situation that has heretofore been ignored, then the same transformation of the profile of the unreacted reactant (RA) can also yield information regarding the reaction network.

As was the case in the IDIMP and TRIMP studies, the nature of the “gas-phase holdup” can affect the shape of these profiles. However, in this case the effect is far less severe. The relationship between the “gas-phase holdup” and the  $\alpha(\text{product})$  response (in the case of irreversible adsorption/desorption) has been previously derived (39).

In our case the semilogarithmic plot of the  $\bar{\alpha}$  function versus time for the production of both N<sub>2</sub> and N<sub>2</sub>O is shown with a standard Ar response in Fig. 8. Both of these are convex, and thus both sets of intermediates (of N<sub>2</sub> and N<sub>2</sub>O) must have buffer states or possibly are formed from parallel mechanisms such as those detailed in the fourth row of Table 5. Qualitative analysis of the profiles indicates that the probability of the latter is not high, and therefore we must incorporate some buffer states within the reaction mechanism for the production of N<sub>2</sub> and N<sub>2</sub>O. It must also be pointed out that these cannot be the same species for the formation of N<sub>2</sub> and N<sub>2</sub>O.

It is seen that the N<sub>2</sub>O profile is far sharper than that of the N<sub>2</sub>. This is to be expected since the transient in N<sub>2</sub>O is itself far quicker than that for N<sub>2</sub> (N<sub>2</sub>O is the isotopically first product). A value of 4 in the semilogarithmic plot is indicative of 99% transference of the heavy (<sup>15</sup>N) isotope into the product molecules.

## PROPOSED MECHANISM

From this analysis, we can propose a mechanism for the conversion of the NO/H<sub>2</sub>/O<sub>2</sub> reaction mixture to N<sub>2</sub>/N<sub>2</sub>O and NO<sub>2</sub> over Pt/SiO<sub>2</sub> catalysts, and there are several points which we can determine from our analysis to be correct. These are:

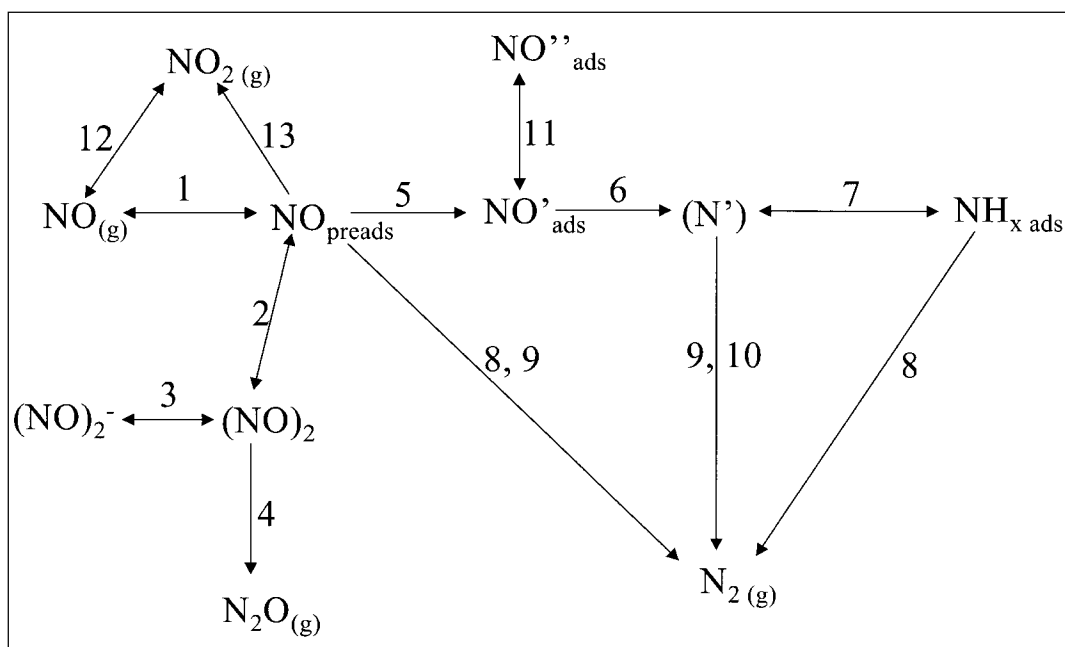
- the experiments show that N<sub>2</sub>O is “isotopically first” and the proposed mechanism must be consistent with this;
- from the TRIMP analysis we know that there are two routes to N<sub>2</sub> formation; furthermore, we can describe the features of the “final surface steps” involved in each of these routes ((a) for example an interaction between a weakly adsorbed species which is in rapid equilibrium with the gas-phase NO and a chemisorbed species, each of which donates one single N atom to the final N<sub>2</sub> product; (b) the interaction of two equivalent chemisorbed species on the surface, each donating one single N atom to the N<sub>2</sub> product);
- the relative contributions of each of these routes to N<sub>2</sub> formation;
- the route to NO<sub>2</sub> formation is through both gas-phase and surface reactions;
- the route to N<sub>2</sub>O formation is through a final step involving a coupled intermediate (which donates two N atoms to the final N<sub>2</sub> product) on the surface;
- N<sub>2</sub>O formation requires the presence of a species in reversible equilibrium with the gaseous NO;
- there are buffer states on the surface for intermediates in the formation of N<sub>2</sub> and N<sub>2</sub>O and these cannot be the same for both products.

Using this information we can consider the possible chemical nature of the various intermediates and the types of paths the intermediates follow to the final products. It must be remembered that this information gives a formalism to the intermediates (we know how many N atoms yielded per intermediate to product), the reaction steps (we know the nature of the final interactions), and the network mechanism (we know that there is a buffer state), but it cannot shed light on the absolute chemical nature of the intermediates or their reaction. For this information a more detailed study involving *in situ* spectroscopic techniques would be needed.

Scheme 1 shows a plausible reaction network in which, for convenience, we have allocated precise descriptions to the various species. Again, we stress that the actual chemical nature of the proposed surface species is speculative, but those chosen seem intuitively reasonable. For example, we refer to an NO<sub>preads</sub> species. We know that this species leads to N<sub>2</sub> and N<sub>2</sub>O production, that it is weakly bound to the surface, that it donates one N atom in N<sub>2</sub> formation, and that it is in rapid equilibrium with the gas phase. However, we do not know its exact chemical form.

The mechanism of the reaction has similarities to that previously proposed for the NO/H<sub>2</sub> reaction in the absence of O<sub>2</sub> although there are important differences of detail. The main feature is that N<sub>2</sub> and N<sub>2</sub>O are formed in parallel through a weakly adsorbed surface species which is in rapid equilibrium with the gaseous NO (represented as NO<sub>preads</sub>).

With respect to N<sub>2</sub>O formation we can say that the reaction is very fast, requires a weakly adsorbed species, has a



SCHEME 1. Network of NO conversion into N<sub>2</sub>O and N<sub>2</sub> over 5% Pt/SiO<sub>2</sub> in the NO/O<sub>2</sub>/H<sub>2</sub> reaction as derived from SSITK Analysis.

surface intermediate which contains two N atoms, and has a buffer step.

The mechanism presented in Scheme 1 shows the adsorption of NO to form a preadsorbed state (step 1). This then dimerises (step 2) to form an (NO)<sub>2</sub>-type species that can be stabilised by the addition of an electron (NO)<sub>2</sub><sup>-</sup> (step 3). The dimer can also decompose to form N<sub>2</sub>O (step 4). We know that the final intermediate before the formation of N<sub>2</sub>O on the surface gives two N atoms to the N<sub>2</sub>O molecule, so the proposition of a dimeric (NO)<sub>2</sub> species is not unreasonable. We also know that there is a buffer state on the route to N<sub>2</sub>O formation. We have represented this as the dimeric species stabilised by the addition of an electron (NO)<sub>2</sub><sup>-</sup>. This intermediate has been previously proposed as an intermediate in N<sub>2</sub>O formation from NO over Pt-based catalysts (40).

In the formation of N<sub>2</sub> we must account for two routes. Again, all we can definitely say about the first route is that there is an interaction between a gaseous (or physisorbed) NO molecule with a surface species containing one N atom and that this interaction leads to ~85% of the N<sub>2</sub> formed from the reaction. This can be envisaged as step 8, where the physisorbed NO molecule reacts with a reduced N-containing species (NH<sub>x</sub>) on the surface. The reduced N-containing species must be formed from the chemisorption of the preadsorbed NO molecule (step 5) and the reduction of this species (steps 6 and 7). Another possibility for this "type" of production can be chemically represented as the interaction of the physisorbed NO with another "N" species, e.g., formed via the decomposition of the NO<sub>ads</sub> species in Step 6, as the type 1 route, in an NO<sub>preads</sub> + N<sub>ads</sub> → N<sub>2</sub> + O<sub>ads</sub> reaction. This form of N<sub>2</sub> production is represented as step 9 in the scheme.

The second mechanism of N<sub>2</sub> formation (accounting for ~15% of the N<sub>2</sub> formed) is via the interaction of two identical surface intermediates, both of which give one N atom to the N<sub>2</sub> product. This is represented in the scheme as step 10 and can be thought of as N<sub>ads</sub> + N<sub>ads</sub> → N<sub>2</sub>. Again, we cannot exclude other interactions leading to this "type" of production, e.g., NO<sub>ads</sub> + NO<sub>ads</sub> → N<sub>2</sub> or NH<sub>xads</sub> + NH<sub>xads</sub> → N<sub>2</sub>. All we can definitely state is that there is a route of formation to N<sub>2</sub> which involves the interaction of two equivalent surface species. We also know that there is a buffer state present somewhere in the reaction scheme, and this is represented as NO''—formed in step 11.

The formation of NO<sub>2</sub> is also considered in the scheme as coming from gas-phase NO (step 12) or the interaction of the chemisorbed NO molecule with O<sub>ads</sub> on the surface (step 13).

The presence of different forms of chemisorbed NO and atomic N species on Pt has been reported previously using an SERS technique (41). Spectroscopic evidence for the presence of (NO)<sub>2</sub> intermediates has been presented for NO adsorption on Pt (42). NH<sub>x</sub> species have also been reported on Pt by using a HREELS technique (43). Therefore,

although in our mechanistic analysis we cannot identify specific surface intermediates, all those which are postulated in Scheme 1 are known to exist under different conditions on Pt catalysts. However, these experimental observations are obtained under different reaction conditions, and our analysis simply gives formal identities to the individual species.

## CONCLUSIONS

A mechanism has been proposed for the NO/O<sub>2</sub>/H<sub>2</sub> reaction over Pt/SiO<sub>2</sub>. The main products (N<sub>2</sub> and N<sub>2</sub>O) are formed in a parallel mechanism through a preadsorbed NO intermediate. This involves the formation of N<sub>2</sub>O as a very rapid process which moves through an intermediate containing two N atoms on the surface. There are two routes for the formation of N<sub>2</sub>. One is through an impact mechanism (where physisorbed NO interacts with a reduced N-containing species on the surface). This is a type 1 production and leads to ~85% of the N<sub>2</sub> formed. The second route involves two identical species on the surface, which combine to form N<sub>2</sub> (both species giving one N atom to the final product). This is a type 2a production and leads to ~15% of the N<sub>2</sub> formation. The contribution of the latter route is decreased relative to its contribution in the NO/H<sub>2</sub> reaction, and correspondingly the contribution of the former (impact) route is increased. Every N<sub>2</sub> molecule formed takes an average of 1.15 N atoms from the surface and an average of 0.85 N atoms from gaseous NO.

We conclude that the effect of the excess of O<sub>2</sub> on the NO/H<sub>2</sub> reaction is to remove the higher temperature deNO<sub>x</sub> activity, suppress NH<sub>3</sub> formation, form NO<sub>2</sub>, and decrease the *overall* amount of N<sub>2</sub> and N<sub>2</sub>O formed. These effects can be thought of as being due to competitive adsorption between the NO and O<sub>2</sub> (or between the H<sub>2</sub> and the O<sub>2</sub>). The overall mechanisms of N<sub>2</sub> and N<sub>2</sub>O formation are unchanged although the relative contributions of different types of N<sub>2</sub> production are different.

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